

Shape memory behavior of Ti-rich Ti-Ni thin films formed by sputtering

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Abstract. The shape memory behavior of Ti-rich Ti-Ni thin films (Ti-45.2, 47.0, 47.9 at.%Ni) annealed at 773, 823, 873K for 1h was investigated. Transmission electron microscopy revealed that Ti-45.2at. %Ni thin films contain randomly oriented Ti_2Ni particles, while the other two films contain Ti_2Ni precipitates with the same orientation as that of the TiNi matrix. In addition to the Ti_2Ni precipitates, GP zones were also observed in a Ti-47.9at. %Ni thin film annealed at 773K for 1h. Every specimen showed a two-stage transformation in a low stress range. The martensitic transformation temperature was found to decrease with increasing Ti content and decreasing annealing temperature. However, thin films containing GP zones showed significantly low transformation temperatures in spite of a low Ti content. The residual strain was found to increase with increasing Ti content and decreasing annealing temperature. The transformation strain was found to increase with decreasing Ti content and annealing temperature. In particular, the thin films containing GP zones showed a large transformation strain. The transformation temperatures of Ti-rich Ti-Ni thin films were generally higher than those of Ni-rich Ti-Ni thin films.

1. INTRODUCTION

Recently sputter-deposited thin films of Ti-Ni are expected to be used as microactuators for micromachines such as micromanipulators and fluid microvalves[1-5]. In the past years, the present authors have been successful in quantitatively evaluating shape memory effect[6,7], stability of shape memory effect against thermal cycles[8], two way shape memory effect[9], superelasticity[10] and mechanical properties[11]. We found that the shape memory characteristics and mechanical properties of sputter-deposited Ti-Ni thin films are comparable or even superior to those of bulk specimens[12]. Especially, it has been found that peculiar microstructures formed in Ti-rich Ti-Ni thin films[13] improve the shape memory characteristics[14] and mechanical properties[15]. In addition, it is known that the transformation temperatures of Ti-rich Ti-Ni thin films are higher than those in Ni-rich Ti-Ni films[16]. These findings have stimulated interests in Ti-rich Ti-Ni thin films rather than Ni-rich Ti-Ni thin films from the viewpoint of both practical and fundamental aspects. The effect of heat treatment on the shape memory behavior of Ti-48.2at.%Ni thin films has been already reported by the present authors[17], but the composition effect on the shape memory behavior has not been investigated systematically, though the composition effect on the transformation behavior has been reported by Gyobu et al.[16]. In this paper the effects of composition and heat treatment on the shape memory behavior of Ti-rich Ti-Ni thin films were investigated.

2. EXPERIMENTAL

Ti-rich Ti-Ni thin films of Ti-45.2, 47.0 and 47.9at. %Ni were deposited on glass substrates with a carousel type magnetron sputtering apparatus shown in Fig. 1. In this study two targets of Ti and Ti-50at.%Ni were used to control the film composition and the DC powers were controlled independently; the Ti target was varied from 305 to 420W while the Ti-50at.%Ni target was kept at 800W. The substrate temperature was 523K and Ar gas pressure was 0.3Pa. The substrate holder was rotated at 60rpm to obtain composition homogeneity during sputtering. The deposition was carried out for 2h and the film thickness ranged from 6 to 8 μm .

The film composition was determined by EPMA analysis using two kinds of standard specimens, Ti-50at.%Ni and Ti-51at.%Ni. After sputtering, they were removed from the glass substrates and then annealed at three different temperatures, 773, 823 and 873K for 1h to produce crystallization. These heat treatments were carried out in a vacuum furnace equipped with infrared lamps. The microstructure of the films was observed with a transmission electron microscope. Thin foils for the transmission electron microscopy were prepared by double-jet electropolishing in an electrolyte consisting of 95% acetic acid and 5% perchloric acid by volume. The transmission electron microscopy studies were carried out at 423K to avoid the formation of the martensitic phase and R-phase.

The shape memory behavior of the annealed films was measured with a small tensile tester equipped with an automatically controlled heater. The size of the sample used for this test was $0.4 \times 5 \text{ mm}^2$ (gauge portion) and the thickness was from 6 to 8 μm . This test involved loading a sample at a high temperature, cooling it down to 143K at a rate of -10 K min^{-1} and heating it back to the original temperature at a rate of 10 K min^{-1} . A series of strain-temperature measurements under various constant stresses was carried out with one sample by varying the stress from 20 to 120MPa in steps of 20 MPa and then from 120 to 600 MPa in steps of 40 MPa. The transformation temperatures were obtained by the tangential method in the strain-temperature curves as described previously[17].

3. RESULTS AND DISCUSSION

3.1 Microstructure

The grain size in annealed thin films was not affected by heat treatment, but it decreased with increasing Ti content, being roughly $1 \mu\text{m}$ for Ti-45.2at.%Ni, $3 \mu\text{m}$ for 47.0at.%Ni and $5 \mu\text{m}$ for 47.9at.%Ni. Every film contains precipitates within the TiNi grains. Transmission electron microscopy revealed that Ti-45.2at.%Ni thin films contain randomly oriented Ti_2Ni particles[18], while the other films, Ti-47.0 and 47.9at.%Ni thin films, contain Ti_2Ni precipitates with the same orientation as that of the TiNi matrix[13]. In addition to the oriented Ti_2Ni , a Ti-47.9at.%Ni thin film annealed at 773K for 1h shows G.P. zones[19]. These GP zones disappeared after annealing at 823K for 1h and only Ti_2Ni precipitates remained in the films annealed at 823K and 873K [13]. The amount of Ti_2Ni precipitates increases with increasing Ti content and their size increases with increasing annealing temperature. The Ti_2Ni precipitates also tend to segregate at the grain boundaries with increasing annealing temperature[17].

3.2 Shape memory behavior

3.2.1 Ti-45.2at.%Ni thin film

Fig. 2 shows the strain-temperature curves under various constant stresses of Ti-45.2 at.%Ni thin films annealed at 773, 823 and 873K for 1h. The thin film annealed at 773K shows a two-stage elongation on cooling and a two-stage contraction on heating respectively[17]. The elongation on cooling is attributed to the R-phase transformation at a high temperature and the martensitic transformation at a low temperature, while the contraction on heating attributable to the reverse martensitic transformation at a

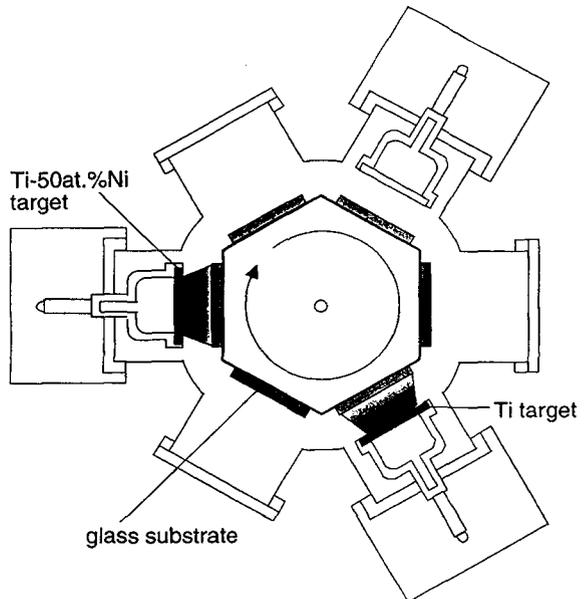


Fig.1 Schematic illustration of carousel type magnetron sputtering apparatus

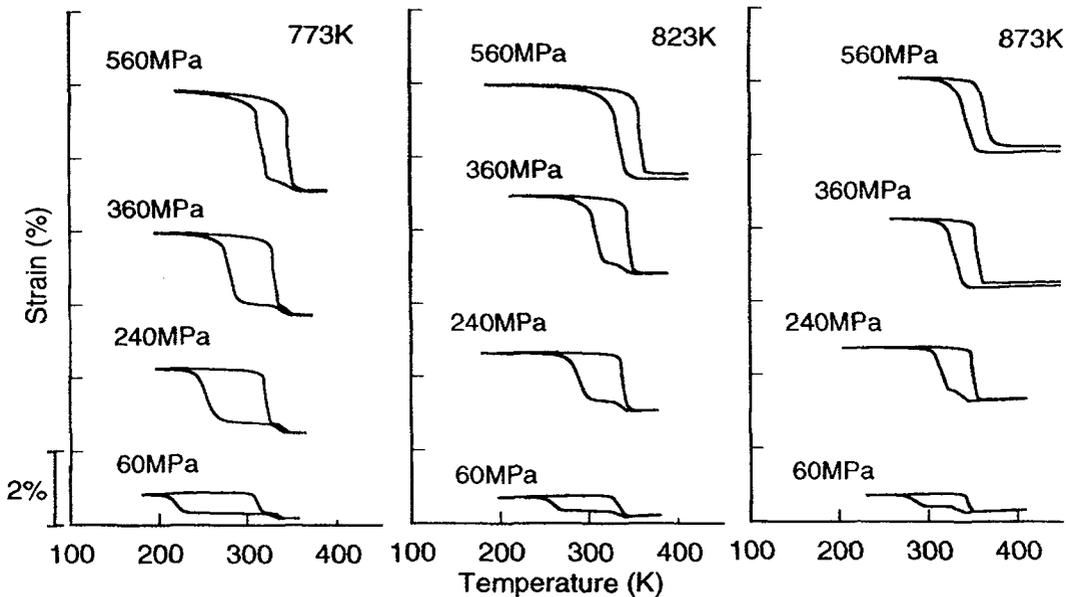


Fig. 2 Strain-temperature curves under various stresses of Ti-45.2at.%Ni thin films annealed at 773K, 823K and 873K for 1h

low temperature and the reverse R-phase transformation at a high temperature. The temperature for each transformation increases with increasing stress. For example, the martensitic transformation start temperature (M_s) increases considerably from 209K at 60MPa to 310K at 560MPa, while the R phase transformation start temperature (R_s) slightly increases from 336K at 60MPa to 357K at 560MPa. Since the martensitic transformation temperature has stronger dependence on stress than the reverse martensitic transformation temperature, the temperature hysteresis decreases with increasing stress. The strain caused by the forward transformations recovered by the reverse transformations completely for the thin film annealed at 773K. The transformation strain was 2.8% at 560MPa, being a little small compared with those of Ti-47.0at.%Ni and -47.9at.%Ni films. These shape memory characteristics of the Ti-45.2at.%Ni thin film annealed at 773K for 1h can be explained by the existence of fine Ti_2Ni particles as follows. The fine Ti_2Ni particles in the thin film annealed at 773K are considered to resist the deformation accompanied with the martensitic transformation and thus reduce the transformation temperature. They also suppress a plastic deformation associated with the transformation and the preferential orientation of the martensite variants, resulting in a small residual strain and a small transformation strain. Annealing at high temperatures of 823 and 873K raises the martensitic transformation temperature. This increase in the martensitic transformation temperature results from the coarsening and grain boundary segregation of the Ti_2Ni particles. When the martensitic transformation temperature is high like in the thin films annealed at 823K and 873K, the two-stage contraction cannot be seen in the heating curve and a single-stage contraction due to the reverse martensitic transformation alone appears instead. Furthermore, at high stresses (560MPa for the 823K annealing, 360MPa for the 873K annealing) a single-stage elongation due to the martensitic transformation occurs instead of the two-stage elongation. Annealing at 873K reduces the transformation strain from 2.76% for 773K to 2.01% for 873K and increases the residual strain. The decrease in the transformation strain and the increase in the residual strain are ascribed to the coarsening and grain boundary segregation of the Ti_2Ni particles.

3.2.2 Ti-47.0at.%Ni thin films

Fig. 3 shows the strain-temperature curves under various constant stresses of Ti-47.0at.%Ni thin films annealed at 773, 823 and 873K for 1h. It was found that, compared with the shape memory behavior of

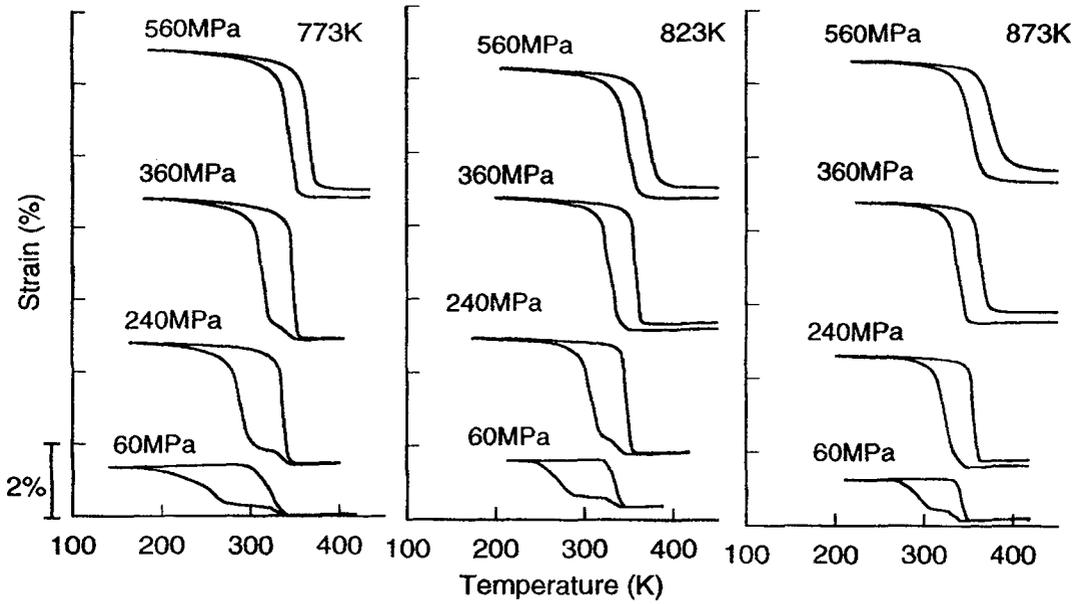


Fig. 3 Strain-temperature curves under various stresses of Ti-47.0at.%Ni thin films annealed at 773K, 823K and 873K for 1h

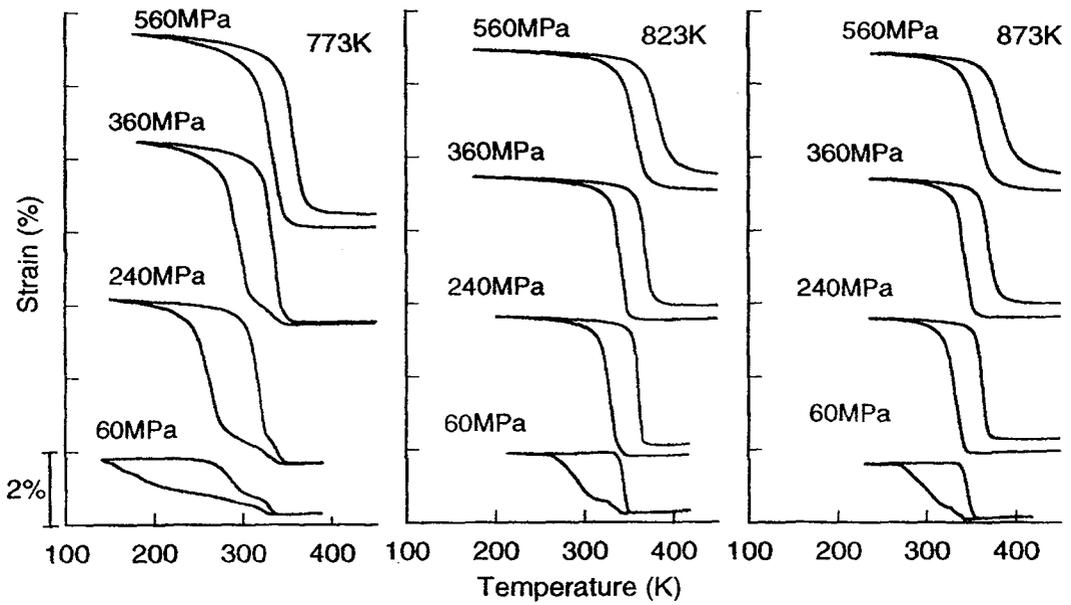


Fig. 4 Strain-temperature curves under various stresses of Ti-47.9at.%Ni thin films annealed at 773K, 823K and 873K for 1h

the Ti-45.2at.%Ni thin films, the transformation temperatures are high and the transformation strains and residual strains are large. This comes from a smaller amount of Ti_2Ni precipitates and larger grain size. Like in the Ti-45.2at.%Ni thin films, the M_s temperature increases with increasing annealing temperature. The transformation strain at 560MPa decreases with increasing annealing temperature. Further, the residual strain appears at 560MPa for 773K annealing and at 360MPa for 823K annealing and at 240MPa for 873K annealing respectively. Apparently the coarsening and grain boundary segregation of Ti_2Ni precipitates are responsible for the degradation in the shape memory effect.

3.2.3 Ti-47.9at.%Ni thin films

Fig. 4 shows the strain-temperature curves under various constant stresses of Ti-47.9at.%Ni thin films annealed at 773, 823 and 873K for 1h. The interesting thing in this figure is the shape memory behavior of the thin film annealed at 773K for 1h. The transformation temperatures of this film are significantly lower than those of Ti-47.0at.%Ni thin films in spite of less Ti. Besides the plastic strain is small though the transformation strain is considerably larger than those of Ti-47.0at.%Ni thin films. This peculiar shape memory behavior comes from the existence of GP zones. The strain field formed around the GP zones suppresses the deformation associated with the transformation, thus resulting in low martensitic transformation temperatures. The same strain field also suppresses the movement of dislocations while the reorientation of variants, i.e. the movement of twin boundary, is easy since the lattice is continuous. As shown in the figure, the disappearance of GP zones after annealing at 823K increases the residual strain and the martensitic transformation temperature, and decreases the transformation strain drastically. In addition to the existence of GP zones, the composition of the matrix may affect the transformation temperatures in the film annealed at 773K since the matrix in the film is likely to be supersaturated in Ti. However, the effect of the matrix composition is not clear for Ti-rich composition[12] and hence it cannot be discussed in detail.

3.2.4 Composition dependence of transformation temperature

Fig. 5 shows the composition dependence of the martensitic transformation start temperature. For the films annealed at 823 and 873K, the martensitic transformation start temperature decreases with increasing Ti content. This is due to an increase of the Ti_2Ni amount. However, a Ti-47.9at.%Ni thin film annealed at 773K for 1h shows a lower martensitic transformation temperature than a Ti-47.0at.%Ni thin film annealed at the same temperature in spite of the small amount of Ti_2Ni . This decrease in the martensitic transformation start temperature can be explained by the existence of GP zones as discussed in the previous section. The reverse martensitic transformation temperature was also found to show similar dependence on the composition and annealing temperature, but the effect is small compared with the martensitic transformation temperature. The thermal hysteresis, therefore, decreases with increasing annealing temperature and Ni content. In contrast to the martensitic transformation temperatures, the R phase transformation temperatures of annealed thin films are almost constant except for a Ti-47.9at.%Ni thin film with GP zones, which shows a low R-phase transformation temperature. The fact that Ti-rich Ti-Ni thin films show relatively high R-phase transformation temperatures (approximately 340K for the R-phase transformation start temperature) irrespective of composition and annealing conditions seems favorable for the practical use.

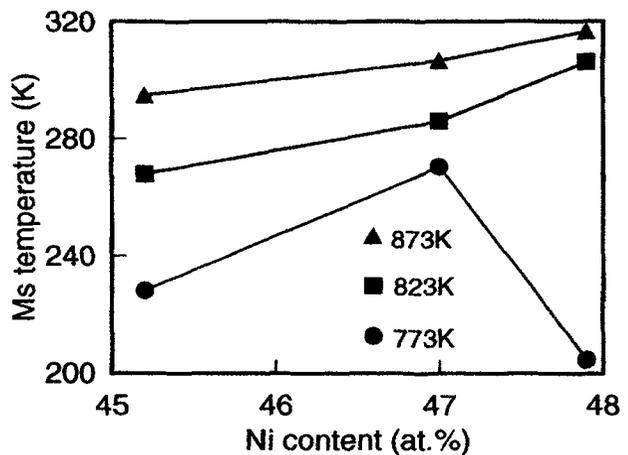


Fig.5 Composition dependence of the martensitic transformation start temperature(M_s) of Ti-rich Ti-Ni thin films annealed at 773K, 823K and 873K

4. CONCLUSION

Ti-rich Ti-Ni thin films of Ti-45.2at.%, 47.0at.%Ni and 47.9at.%Ni were annealed at 773, 823 and 873K and their shape memory behaviors were investigated. The obtained results were as follows.

(1) The martensitic transformation temperature of thin films with Ti₂Ni precipitates alone decreases with increasing Ti content and decreasing annealing temperature, but a Ti-47.9at.%Ni film annealed at 773K for 1h shows a low martensitic transformation temperature owing to the existence of GP zones.

(2) The R-phase transformation temperatures of thin films with Ti₂Ni precipitates alone are almost constant, but it is low in a Ti-47.9at.%Ni film with GP zones.

(3) The residual strain decreases with decreasing Ti content and increasing annealing temperature, but a thin film annealed at 773K for 1h shows a small residual strain owing to the existence of GP zones.

(4) The transformation strain increases with decreasing Ti content and decreasing annealing temperature. Especially, a Ti-47.9at.%Ni film with GP zones shows a large transformation strain.

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